# FLIGHT PLAN BASED AIRCRAFT CONFLICT DETECTION METHOD 

${ }^{1}$ Nadir Agayev, ${ }^{2}$ Nasraddin Isgandarov<br>${ }^{1,2}$ National Aviation Academy, Baku, Azerbaijan


#### Abstract

Early detection of conflicts between aircraft is the main purpose of air traffic management. This article provides an algorithm for calculating future aircraft geographical coordinates and conflict detection based on flight plans using the Vincenty formula. Finally, the experimental results are listed in tabular form.


Keywords- Conflict detection; flight plan; geographical coordinate; Vincenty formula

## I. INTRODUCTION

Improvements to air traffic control (ATC) systems could help prevent aircraft to aircraft and aircraft to other obstacles conflict. To achieve this goal, the ATC systems provide information indicating aircraft's coordinates, process and manage flight plans, detect conflicts, and implement controller requests. The increased amount of air traffic requires more effective conflict detection methods. Conflict prediction accuracy allows for optimal maneuvering. Investigations of different aircraft conflict prediction and resolution methods [1,2 and 3] show that the main factor for an accurate resolution algorithm is accurate calculation of predicted aircraft coordinates. A mathematical model of the aircraft flight [4] and the algorithms for medium-term conflict detection $[5,6]$ are accurate for short-term predicted states of an aircraft, and these algorithms are better used for short-term conflict detection[7]. In medium-term conflict detection [8], forecasting aircraft flight for 20 minutes using these methods leads to certain errors because aircraft will fly long distances and aircraft trajectory is parallel to the curvature of the earth. Thus, the geodetic (or geographical) coordinate system is more suitable for determining coordinates. In [9] is given the method for calculating aircraft trajectory in a geodetic coordinate system. For calculation using the Vincenty formula [10]. Investigations show that the Vincenty formula is more accurate [11]. In this article, we will provide the algorithm for calculating future geographical aircraft coordinates and conflict detection based on flight plans using the Vincenty formula.

## II. FLIGHT PLAN BASED AIRCRAFT CONFLICT DETECTION ALGORITHM

Let's look at a simple model to solve the problem. For this, we can use any flight. Let's suppose that, aircraft A1's trajectory, according to the flight plan, passes through points B1, B2, and B5, and aircraft A2's trajectory passes through points B3, B2, and B4 in sector S (Fig. 1). These points are fixed points and their geographical coordinates are known in advance [12].

Let's calculate coordinates for aircraft A1 between points B1 and B2 and for aircraft A2 between points B3 and B2 and use the conflict detection algorithm for these aircraft.

First, we must extract information about the flights for both aircraft from their flight plans [13]. We take cruising speed, altitude, and aircraft route information from flight plans. Let's use the following for calculation:
$V_{A 1}, V_{A 2}$ - the speed of aircrafts A1 and A2 according to flight plan;
$H_{A 1}, H_{A 2}$ - the altitude of aircrafts A1 and A2 according to flight plan;
$B 1\left(\varphi_{B 1}, \lambda_{B 1}\right), B 2\left(\varphi_{B 2}, \lambda_{B 2}\right), B 3\left(\varphi_{B 3}, \lambda_{B 3}\right), B 4\left(\varphi_{B 4}, \lambda_{B 4}\right), B 5\left(\varphi_{B 5}, \lambda_{B 5}\right)$ - geographical coordinates of points according to flight plan.
$t_{A 1}$-aircraft A1's entry time into S sector from point B 1 . This is given in advance from the neighboring sector.
$t_{A 2}$-aircraft A2's entry time into S sector from point B3. This is given in advance from the neighboring sector.
$A 1\left(\varphi_{A 1}, \lambda_{A 1}\right), A 2\left(\varphi_{A 2}, \lambda_{A 2}\right)-$ geographical coordinates of aircrafts A1 and A2.


Fig 1. ATC sector
As mentioned, we will use the Vincenty formula for calculations. This formula is intended for calculations on the surface of earth. Thus, we will add aircraft altitude to the earth radius. To simplify calculations, we will separately describe Vincenty's direct and inverse methods and give dependence to output parameters from input parameters.

[^0]Vincenty's inverse method: Vincenty's inverse method calculates geodesic distance and start and final azimuths for two points using geodesic coordinates.

The algorithm of Vincenty's inverse method:

1. Included: $\varphi_{1}, \varphi_{2}, \lambda_{1}, \lambda_{2}, \mathrm{H}$ input parameters. $\left\{\varphi_{1}, \varphi_{2}-\right.$ geodesic latitude, $\lambda_{1}, \lambda_{2}-$ geodesic longitude, H aircraft altitude $\}$.
2. Included: a1, b1, $\boldsymbol{\varepsilon}\{$ Earth ellipsoid major and minor radius and calculating error \}
3. Calculates:
$\mathrm{a}=\mathrm{a} 1+\mathrm{H} ; \quad \mathrm{b}=\mathrm{b} 1+\mathrm{H}$;
$\mathrm{f}=(\mathrm{a}-\mathrm{b}) / \mathrm{a}$; \{flattening \}
$L=\lambda_{1}-\lambda_{2} ;\{$ longitude difference $\}$
$\mathrm{U}_{1}=\operatorname{atan}\left((1-\mathrm{f}) \cdot \tan \varphi_{1}\right)$;
$\mathrm{U}_{2}=\operatorname{atan}\left((1-\mathrm{f}) \cdot \tan \varphi_{2}\right)$;
$\lambda=\mathrm{L}$; \{first approximation $\}$
4. Beginning of the period
5. Calculates:
$\sin \sigma=\sqrt{\left(\cos U_{2} \cdot \sin \lambda\right)^{2}+\left(\cos U_{1} \cdot \sin U_{2}-\sin U_{1} \cdot \cos U_{2} \cdot \cos \lambda\right)^{2}}$
$\cos \sigma=\sin \mathrm{U}_{1} \cdot \sin \mathrm{U}_{2}+\cos \mathrm{U}_{1} \cdot \cos \mathrm{U}_{2} \cdot \cos \lambda ;$
$\sigma=\operatorname{atan} 2(\sin \sigma, \cos \sigma) ;$
$\sin \alpha=\cos \mathrm{U}_{1} \cdot \cos \mathrm{U}_{2} \cdot \sin \lambda / \sin \sigma ;$
$\cos ^{2} \alpha=1-\sin ^{2} \alpha$;
$\cos 2 \sigma_{\mathrm{m}}=\cos \sigma-2 \cdot \sin \mathrm{U}_{1} \cdot \sin \mathrm{U}_{2} / \cos ^{2} \alpha$;
$\mathrm{C}=\mathrm{f} / 16=\cos ^{2} \alpha=\left[4+\mathrm{f}=\left(4-3=\cos ^{2} \alpha\right)\right]$;
$\lambda^{\prime}=\mathrm{L}+(1-\mathrm{C}) \cdot \mathrm{f} \cdot \sin \alpha=\left[\sigma+\mathrm{C} \cdot \sin \sigma=\left[\cos 2 \sigma_{\mathrm{m}}+\mathrm{C} \cdot \cos \sigma\right.\right.$
$\left.\left.\cdot\left(-1+2 \cdot \cos ^{2} 2 \sigma_{\mathrm{m}}\right)\right]\right]$;
6. End of the period
7. If $\left(\left|\lambda^{\prime}-\lambda\right|>\varepsilon\right)$ then accept $\lambda=\lambda^{\prime}$ do step 5;
8. Else
9. Calculates:
$\mathrm{u}^{2}=\cos ^{2} \alpha \cdot\left(\mathrm{a}^{2}-\mathrm{b}^{2}\right) / \mathrm{b}^{2} ;$
$\mathrm{A}=1+\mathrm{u}^{2} / 16384 \cdot\left[4096+\mathrm{u}^{2} *\left[-768+\mathrm{u}^{2} *\left(320-175 * \mathrm{u}^{2}\right)\right]\right]$;
B $=u^{2} / 1024 \cdot\left[256+u^{2} \cdot\left[-128+u^{2} \cdot\left(74-47 \cdot u^{2}\right)\right]\right]$;
$\Delta \sigma=\mathrm{B}^{*} \sin \sigma^{*}\left[\cos 2 \sigma_{\mathrm{m}}+\mathrm{B} / 4 \cdot\left[\cos *\left(-1+2 * \cos ^{2} 2 \sigma_{\mathrm{m}}\right)-\mathrm{B} / 6\right.\right.$
$\left.\left.* \cos 2 \sigma_{\mathrm{m}}{ }^{*}\left(-3+4 * \sin ^{2} \sigma\right) \cdot\left(-3+4 * \cos ^{2} 2 \sigma_{\mathrm{m}}\right)\right]\right]$;
10. Calculates output parameters:
$\mathrm{S}=\mathrm{b} \cdot \mathrm{A} \cdot(\sigma-\Delta \sigma) ;\{\mathrm{S}-$ distance $\}$
$\alpha_{1}=\operatorname{atan} 2\left(\cos U_{2} * \sin \lambda, \cos U_{1} * \sin U_{2}-\sin U_{1} * \cos U_{2}\right.$ $\cdot \cos \lambda) ;\left\{\alpha_{1}-\right.$ start azimuth $\}$
$\alpha_{2}=\operatorname{atan} 2\left(\cos \mathrm{U}_{1} * \sin \lambda,-\sin \mathrm{U}_{1} * \cos \mathrm{U}_{2}+\cos \mathrm{U}_{1} * \sin \mathrm{U}_{2}\right.$
$\cdot \cos \lambda) ; \quad\left\{\alpha_{2}-\right.$ final azimuth $\}$

## 11. End of algorithm.

Vincenty's direct method: Vincenty's direct method calculates final point coordinates and azimuth using start point coordinate and azimuth and distance between starting and final points.

## The algorithm of Vincenty's direct method:

1. Included: $\varphi_{1}, \lambda_{1}, \mathrm{H}, \mathrm{S}, \alpha_{1}$ input parameters $\left\{\varphi_{1}-\right.$ geodesic latitude, $\lambda_{1}$ - geodesic longitude, H - aircraft altitude, S -geodesic distance, $\alpha_{1}$-start azimuth $\}$.
2. Included: a1, b1, $\mathcal{E}$ \{Earth ellipsoid major and minor radius and calculating error \}
3. Calculates:
$\begin{aligned} & \mathrm{a}=\mathrm{a} 1+\mathrm{H} ; \mathrm{b}=\mathrm{b} 1+\mathrm{H} ; \\ & \mathrm{f}=(\mathrm{a}-\mathrm{b}) / \mathrm{a} ;\{\mathrm{flattening}\} \\ & \tan \mathrm{U}_{1}=(1-\mathrm{f}) \cdot \tan \varphi_{1} ;\end{aligned}$
$\cos U_{1}=1 / \sqrt{\left(1+\tan ^{2} U_{1}\right)} ;$
$\sin \mathrm{U}_{1}=\tan U_{1} \cdot \cos \mathrm{U}_{1} ;$
$\sigma_{1}=\operatorname{atan} 2\left(\tan \mathrm{U}_{1}, \cos \alpha_{1}\right) ;$
$\sin \alpha=\cos \mathrm{U}_{1} \cdot \sin \alpha_{1} ;$
$\cos ^{2} \alpha=1-\sin ^{2} \alpha ;$
$\mathrm{u}^{2}=\cos ^{2} \alpha=\left(\mathrm{a}^{2}-\mathrm{b}^{2}\right) / \mathrm{b}^{2} ;$
$\mathrm{A}=1+\mathrm{u}^{2} / 16384 \cdot\left[4096+\mathrm{u}^{2} \cdot\left[-768+\mathrm{u}^{2} \cdot\left(320-175 \cdot \mathrm{u}^{2}\right)\right]\right] ;$
$\mathrm{B}=\mathrm{u}^{2} / 1024 \cdot\left[256+\mathrm{u}^{2} \cdot\left[-128+\mathrm{u}^{2} \cdot\left(74-47 \cdot \mathrm{u}^{2}\right)\right]\right] ;$
$\sigma=\mathrm{s} / \mathrm{b} \cdot \mathrm{A} ;\{$ first approximation $\}$
4. Start of the period
5. Calculates:
$\cos 2 \sigma_{\mathrm{m}}=\cos \left(2 \cdot \sigma_{1}+\sigma\right)$;
$\Delta \sigma=\mathrm{B}=\sin \sigma=\left[\cos 2 \sigma_{\mathrm{m}}+\mathrm{B} / 4=\left[\cos \sigma=\left(-1+2 \cdot \cos ^{2} 2 \sigma_{\mathrm{m}}\right)\right.\right.$
$\left.\left.-\mathrm{B} / 6 \cdot \cos 2 \sigma_{\mathrm{m}}{ }^{*}\left(-3+4 \cdot \sin ^{2} \sigma\right) \cdot\left(-3+4 \cdot \cos ^{2} 2 \sigma_{\mathrm{m}}\right)\right]\right]$;
$\sigma^{\prime}=\sigma ;$
$\sigma=\mathrm{s} / \mathrm{b}-\mathrm{A}+\Delta \mathrm{\sigma}$;
6. End of period
7. If $\left(\left|\sigma-\sigma^{\prime}\right|>\varepsilon\right)$ then do step 5 .
8. Else
9. Calculates output parameters:
$\varphi_{2}=\operatorname{atan} 2\left(\sin \mathrm{U}_{1} * \cos \sigma+\cos \mathrm{U}_{1} * \sin \sigma * \cos \alpha_{1}\right.$,
$\left.(1-\mathrm{f}) \cdot \sqrt{\left[\sin ^{2} \alpha+\left(\sin U_{1} \cdot \sin \sigma-\cos U_{1} \cdot \cos \sigma \cdot \cos \alpha_{1}\right)^{2}\right]}\right) ;$
$\lambda=\operatorname{atan} 2\left(\sin \sigma \cdot \sin \alpha_{1}, \cos U_{1} \cdot \cos \sigma-\sin U_{1} \cdot \sin \sigma \cdot \cos \alpha_{1}\right) ;$
$\mathrm{C}=\mathrm{f} / 16 \cdot \cos ^{2} \alpha=\left[4+\mathrm{f} \cdot\left(4-3 \cdot \cos ^{2} \alpha\right)\right]$;
$\mathrm{L}=\lambda-(1-\mathrm{C}) \cdot \mathrm{f}=\sin \alpha \cdot\left[\sigma+\mathrm{C}=\sin \sigma=\left[\cos 2 \sigma_{\mathrm{m}}+\mathrm{C} \cdot \cos \sigma\right.\right.$
$\left.\left.\cdot\left(-1+2 \cdot \cos ^{2} 2 \sigma_{m}\right)\right]\right]$;
$\alpha_{2}=\operatorname{atan} 2\left(\sin \alpha,-\sin U_{1} \cdot \sin \sigma+\cos U_{1} \cdot \cos \sigma \cdot \cos \alpha_{1}\right)$;
$\lambda_{2}=\lambda_{1}+L ;$

## 10. End of algorithm

For using Vincenty's direct and Vincenty's inverse methods mark dependence of output parameters from input parameters for Vincenty inverse methods
$S=S_{V i}\left(\varphi_{1}, \varphi_{2}, \lambda_{1}, \lambda_{2}, H\right) ; \alpha_{1}=\alpha_{V i l}\left(\varphi_{1}, \varphi_{2}, \lambda_{1}, \lambda_{2}, H\right) ;$
$\alpha_{2}=\alpha_{V i 2}\left(\varphi_{1}, \varphi_{2}, \lambda_{1}, \lambda_{2}, H\right)$;
For Vincenty's direct method
$\varphi_{2}=\varphi_{V D 2}\left(\varphi_{1}, \lambda_{1}, H, S, \alpha_{1}\right) ; \lambda_{2}=\lambda_{V D 2}\left(\varphi_{1}, \lambda_{1}, H, S, \alpha_{1}\right) ;$
$\alpha_{2}=\alpha_{V D 2}\left(\varphi_{1}, \lambda_{1}, H, S, \alpha_{1}\right) ;$
Aircraft conflict detection algorithm will be as follows:
Step1. Included: Coordinates of points $B 1\left(\varphi_{B 1}, \lambda_{B 1}\right)$, $B 2\left(\varphi_{B 2}, \lambda_{B 2}\right), B 3\left(\varphi_{B 3}, \lambda_{B 3}\right)$, aircraft altitudes $H_{A 1}, H_{A 2}$ and aircraft speeds $V_{A 1}, V_{A 2}$ takes from flight plan; $t_{A 1}, t_{A 2}$ aircraft entry time to the sector S ;
$t$ current time takes from accurate time system;
$\Delta t=5 \mathrm{sec}$ \{Requirement updates information for detection aircraft coordinates maximum 5 second for flight aerodrome zone and maximum 8 second for enroute flight [14], thus we fulfill calculations every 5 second.\}

## Step2. Calculates:

$\alpha_{B 1}=\alpha_{V i 1}\left(\varphi_{B 1}, \varphi_{B 2}, \lambda_{B 1}, \lambda_{B 2}, H_{A 1}\right)$,
$\alpha_{B 3}=\alpha_{V i 1}\left(\varphi_{B 3}, \varphi_{B 2}, \lambda_{B 3}, \lambda_{B 2}, H_{A 2}\right)$
$\left\{\alpha_{B 1}-\right.$ azimuth for flying from point B 1 to point $\mathrm{B} 2, \alpha_{B 3}-$ azimuth for flying from point B3 to point B2 \}.
$\mathrm{n}=0$ \{initial value of calculation step number for aircraft A1\}, $\varphi_{A 1 n}=\varphi_{B 1}, \lambda_{A 1 n}=\lambda_{B 1}\{$ start coordinates for aircraft A1 $\}$
$\alpha_{A 1 n}=\alpha_{B 1}\{$ start azimuth for aircraft A1\}
$\mathrm{m}=0$ \{initial value of calculation step number for aircraft A2\}
$\varphi_{A 2 n}=\varphi_{B 3}, \lambda_{A 2 n}=\lambda_{B 3}\{$ start coordinates for aircraft A2\}
$\alpha_{A 2 n}=\alpha_{B 3}\{$ start azimuth for aircraft A2 \}
$\mathrm{k}=1$ \{initial value for forecast time step number\}
$t_{p k}=t$ \{initial value of forecast time taken equal the current time $\}$

## Step3. Start the period.

Step4. If $\left(t_{A 1} \leq t_{p k}\right)$ then $\{$ this statement shows that the aircraft A1 is entered sector S or not $\}$
[ $g_{A 1}=1 ;$ Do step5;] $\left\{g_{A 1}\right.$ - indicator aircraft A1 coordinate calculations $\}$
Else [ $g_{A 1}=0$; Do step 7;]
Step5. n=n $+1 ; S_{A 1(n-1) A 1 n}=V \cdot \Delta t ;\{$ aircraft A1 flight distance during the $\Delta \mathrm{t}$ time \}

Step6. Calculates: \{calculates coordinates and azimuth for aircraft A1 in time $\left.t_{p k}\right\}$
$\varphi_{A 1 n}=\varphi_{V D 2}\left(\varphi_{A 1(n-1)}, \lambda_{A 1(n-1)}, H_{A 1}, S_{A 1(n-1) A 1 n}, \alpha_{A 1(n-1)}\right) ;$
$\lambda_{A 1 n}=\lambda_{V D 2}\left(\varphi_{A 1(n-1)}, \lambda_{A 1(n-1)}, H_{A 1}, S_{A 1(n-1) A 1 n}, \alpha_{A 1(n-1)}\right) ;$
$\alpha_{A 1 n}=\alpha_{V D 2}\left(\varphi_{A 1(n-1)}, \lambda_{A 1(n-1)}, H_{A 1}, S_{A 1(n-1) A 1 n}, \alpha_{A 1(n-1)}\right)$;
Step7. If $\left(t_{A 2} \leq t_{p k}\right)$ then \{this statement shows that the aircraft A2 is entered sector $S$ or not $\}$
[ $g_{A 2}=1$; Do step 8; ] \{ $g_{A 2}$ - indicator aircraft A2 coordinate calculations $\}$
Else [ $g_{A 2}=0 ;$ Do step 10; ]
Step8. $\mathrm{m}=\mathrm{m}+1 ; S_{\mathrm{A} 2(m-1) A 2 m}=V \cdot \Delta t ;$ aircraft A2 flight distance during the $\Delta \mathrm{t}$ time $\}$
Step9.Calculates: \{calculates coordinates and azimuth for aircraft A2 in time $\left.t_{p k}\right\}$
$\varphi_{A 2 m}=\varphi_{V D 2}\left(\varphi_{A 2(m-1)}, \lambda_{A 2(m-1)}, H_{A 2}, S_{A 2(m-1) A 2 m}, \alpha_{A 2(m-1)}\right)$;
$\lambda_{A 2 m}=\lambda_{V D 2}\left(\varphi_{A 2(m-1)}, \lambda_{A 2(m-1)}, H_{A 2}, S_{A 2(m-1) A 2 m}, \alpha_{A 2(m-1)}\right) ;$
$\alpha_{A 2 m}=\alpha_{V D 2}\left(\varphi_{A 2(m-1)}, \lambda_{A 2(m-1)}, H_{A 2}, S_{A 2(m-1) A 2 m}, \alpha_{A 2(m-1)}\right) ;$
Step10. If $\left(\left(g_{A 1}=1\right)\right.$ and $\left.\left(g_{A 2}=1\right)\right)$ then do step 11;
Else do step 13;
Step 11. If $\left(\left|H_{A 1}-H_{A 2}\right|<H_{l}\right)$ then \{If altitude difference between aircrafts is low allowable limit \} do step 12; Else do step 13;

Step 12. Calculates:
$S_{A 1 A 2}=S_{V i}\left(\varphi_{A 1 n}, \varphi_{A 2 m}, \lambda_{A 1 n}, \lambda_{A 2 m}, H_{A 1}\right)$;
\{Calculates distance between A1 and A2 aircraft. During the calculations for altitude value we can take aircraft A1 altitude or aircraft A2 altitude because this calculations after step 12 and altitude difference between aircrafts is negligible.\}
If $\left(S_{A 1 A 2}<S_{l}\right)$ then [Given the conflict warning between aircraft A1 and A2 after $t_{p k}$ time]
Else do step 13;
Step13. $k=k+1, \quad t_{p k}=t_{p(k-1)}+\Delta t$;
Step14. If $\left(t_{p k}-t \geq 20 \mathrm{~min}\right)$ then end of period;
Else do step 3.

## III. EXPERIMENTAL RESULTS

This article provides an algorithm for aircraft conflict detection based on flight plans using the Vincenty formula. The experimental results are given in Figure 2 and Table1 using the Delphi programming language [15, 16]. In the program the input parameters, point B1 (LatB1 and LonB1), point B2(LatB2 and LonB2), and point B3(LatB3, LonB3) are the geographical coordinates (degree); tA1 and tA2 are entry times in to sector S (hour:min:sec) for aircrafts A1 and A2; HA1 and HA2 are altitude (meter) for aircrafts A1 and A2; VA1 and VA2 are speeds (meter/sec) for aircrafts A1 and A2; Delta $t$ is the calculation step $(\mathrm{sec})$; and Current t is the current time (hour:min:sec). During the calculations, a1 $=6378137 \mathrm{~m}$ (semi-major axis), $\mathrm{b} 1=6356752 \mathrm{~m}$ (semi-minor axis) [17]; and $\varepsilon=1 E-10$ (meter). Output parameters LatA1, LonA1, and DisA1 are aircraft A1's geographical coordinates and flying distance; LatA2, LonA2, and DisA2 are aircraft A2's geographical coordinates and flying distance. It is possible to improve the conflict detection algorithm by including all fixed points for the aircraft and increasing accuracy by calculating aircraft coordinates using radar information.


Fig 2 Simulation results.

International Journal of Latest Research in Science and Technology.

|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LatB1 $\left(^{\circ}\right.$ ) | 38,3465 | 38,9465 | 39,1327 | 40,6327 | 39,0865 | 12,0865 | 23,4535 |
| LonB1( ${ }^{\text {) }}$ | 44,9834 | 45,0231 | 45,2131 | 43,2131 | 44,9834 | 14,8249 | 29,3449 |
| LatB2 $\left(^{\circ}\right.$ ) | 38,7895 | 38,7895 | 37,8895 | 37,8895 | 38,7895 | 13,8105 | 22,4498 |
| LonB2 ${ }^{\circ}$ ) | 46,9548 | 46,4567 | 46,9267 | 46,9267 | 46,9548 | 15,5532 | 31,5532 |
| LatB3 ( ${ }^{\text {) }}$ | 38,4532 | 38,2532 | 38,7632 | 38,7632 | 38,4532 | 11,4614 | 21,4614 |
| LonB3( ${ }^{\circ}$ ) | 45,2342 | 46,2342 | 45,6642 | 45,6642 | 45,2342 | 15,1142 | 30,1142 |
| tA1(time) | 12:05:00 | 15:35:00 | 10:29:00 | 18:10:00 | 00:25:00 | 17:28:00 | 21:56:00 |
| tA2(time) | 12:03:00 | 15:43:30 | 10:32:30 | 18:08:00 | 00:23:00 | 17:31:00 | 22:01:00 |
| HA1(m) | 11000 | 8000 | 8000 | 6000 | 11000 | 6000 | 10000 |
| HA2(m) | 10900 | 11000 | 8100 | 10000 | 11000 | 6100 | 10100 |
| $\mathrm{VA1}(\mathrm{~m} / \mathrm{sec})$ | 250 | 230 | 220 | 220 | 120 | 160 | 260 |
| $\mathrm{VA2}$ ( $\mathrm{m} / \mathrm{sec}$ ) | 150 | 190 | 200 | 240 | 150 | 215 | 230 |
| Current (time) | 12:00:00 | 15:40:00 | 10:30:00 | 18:05:00 | 00:30:00 | 17:30:00 | 21:58:00 |
| LatA1 $\left({ }^{\circ}\right)$ | 38,5609 | 38,5790 | 37,9719 | 39,4199 | 38,8436 | 13,6283 | 22,4779 |
| LonA1 ( ${ }^{\circ}$ ) | 45,9164 | 48,1599 | 46,8159 | 44,9108 | 46,6126 | 15,4757 | 31,4926 |
| DistA1(m) | 85000 | 276000 | 190300 | 198000 | 144000 | 184800 | 245700 |
| LatA2 $\left({ }^{\circ}\right)$ | 38,6063 | 39,8600 | 37,9142 | 37,3025 | 38,8421 | 13,5525 | 22,4023 |
| LonA2 $\left(^{\circ}\right.$ ) | 45,9997 | 46,9116 | 46,8916 | 47,7477 | 47,2379 | 15,5045 | 31,4832 |
| DistA2(m) | 69000 | 188100 | 143000 | 244800 | 180000 | 235425 | 175950 |
| Dist. 2 aircraft(m) | 8846 | 178754 | 9248 | 342146 | 54379 | 8956 | 8435 |
| Conflict situation | After <br> 10 min <br> 35 sec | Not expected | After <br> 14 min <br> 20 sec | Not expected | Not expected | After <br> 19 min <br> 10 sec | After <br> 15 min <br> 40 sec |

## REFERENCES

[1] Н.Б. Агаев, Н.И. Искендеров «Оценка методов моделирования обнаружения конфликтов и принятия решений на основе нечеткой логики» проблеми информатизаці та управлиння, збирник наукових праць: Випуск 1(45). - К.: НАУ, 2014.
[2] Gilles Dowek, Cesar Munoz. Conflict detection and resolution for $1,2, \ldots, \mathrm{~N}$ aircraft. 7th AIAA Aviation Technology, Integration and Operations Conference, 18-20 September 2007, Belfast, Northern Ireland.
[3] Kuchar J. and Yang L., "A Review of Conflict Detection and Resolution Modeling Methods," IEEE Transactions on Intelligent Transportation Systems, Vol. 1, No. 4, December 2000, pp. 179189.
[4] Р.М. Ахмедов, А.А. Бибутов, А.В. Васильев и др. Автоматизированные системы управления воздушным движением: Новые информационные технологии в авиации: Учеб. пособие - СПб. Политехника, 2004.
[5] Alam S., Abbass H.A., Lokan C.J., Ellejmi M., and Kirby S. Computational red teaming to investigate failure patterns in medium-term conflict detection. Defence \& Security Applications Research Centre, University of New South Wales; Australian Defence Force Academy, Canberra, Australia; EUROCONTROL Coorperative Network Design Cooperative Network Division (CND), France 01/2009;
[6] Jean-Marc Alliot, Nicolas Durand. A mathematical analysis of the influence of wind uncertainty on MTCD efficiency. Dans: The Controller, IFATCA - International Federation of Air Traffic Controllers' Associations, Montreal - Quebec, Numéro spécial Meteorology and ATC, Vol. 1 N. Spring 2011, p. 17-19, mars 2011. http://www.alliot.fr/papers/ifatca.pdf
[7] "EUROCONTROL Guidance Material for Short Term Conflict Alert. Appendix A: Reference STCA System" Edition number:2.0, Document identifier: EUROCONTROL-GUID-123, 2009.
[8] EUROCONTROL Specification for Medium-Term Conflict Detection. Edition 1.0, EUROCONTROL-SPEC-139, 2010.
[9] Yong-Kyun Kim, Yun-Hyun Jo, Jin-Won Yun, Taeck-Keun Oh, Hee-Chang Roh, Sang-Bang Choi and Hyo-Dal Park. En-Route Trajectory calculation using Flight Plan Information for Effective Air Traffic Management. Journal of Information Processing Systems, Vol.6, No.3, September 2010.
[10] Vincenty T. (1975). "Direct and inverse solutions of geodesics on the ellipsoid with application of nested equations." Surv. Rev., XXII(176), 88-93.
[11] C.M. Thomas, W.E. Featherstone, "Validation of Vincenty's Formulas for the Geodesic Using a New Fourth-Order Extension of Kivioja's Formula", Journal of Surveying engineering,pp.20-26, Feb., 2005.
[12] ICAO Annex11 to the convention on international civil aviation Air Traffic Services. Thirteenth edition, 2001.
[13] ICAO Doc 4444-ATM/501: Air Traffic Management, fifteenth Edition, 2007.
[14] EUROCONTROL standard document for radar surveillance in enroute airspace and major terminal areas. Edition 1.0, SUR.ET1.ST01.1000-STD-01-01, 1997.
[15] John Barrow. Introducing Delphi Programming: Theory through Practice. Oxford University Press, 2005.
[16] Осипов Д. Л. Базы данных и Delphi. Теория и практика. - СПб.: БХВ-Петербург, 2011.
[17] http://en.wikipedia.org/wiki/World_Geodetic_System.


[^0]:    Publication History
    Manuscript Received
    Manuscript Accepted
    Revision Received

